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July 1992

The following is a list of Intel products that may be used in the manufacture of high end power supplies.

MAGNETIC	9400	328
Modular	10000	340
Media Mail	10150	342
WDC	101500	343
Western	101524	344
Quantum	101525	345
Quantum	101526	346
Quantum	101527	347
Quantum	101528	348
Quantum	101529	349
Quantum	101530	350
Quantum	101531	351
Quantum	101532	352
Quantum	101533	353
Quantum	101534	354
Quantum	101535	355
Quantum	101536	356
Quantum	101537	357
Quantum	101538	358
Quantum	101539	359
Quantum	101540	360
Quantum	101541	361
Quantum	101542	362
Quantum	101543	363
Quantum	101544	364
Quantum	101545	365
Quantum	101546	366
Quantum	101547	367
Quantum	101548	368
Quantum	101549	369
Quantum	101550	370
Quantum	101551	371
Quantum	101552	372
Quantum	101553	373
Quantum	101554	374
Quantum	101555	375
Quantum	101556	376
Quantum	101557	377
Quantum	101558	378
Quantum	101559	379
Quantum	101560	380
Quantum	101561	381
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Quantum	101566	386
Quantum	101567	387
Quantum	101568	388
Quantum	101569	389
Quantum	101570	390
Quantum	101571	391
Quantum	101572	392
Quantum	101573	393
Quantum	101574	394
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Quantum	101577	397
Quantum	101578	398
Quantum	101579	399
Quantum	101580	400
Quantum	101581	401
Quantum	101582	402
Quantum	101583	403
Quantum	101584	404
Quantum	101585	405
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Power Supply Solutions for Flash Memory

CONTENTS	PAGE	CONTENTS	PAGE
1.0 INTRODUCTION	1	5.0 5V V_{CC} SOLUTIONS: CONVERTING UP FROM 3V	14
2.0 FLASH MEMORY POWER REQUIREMENTS	1	5.1 Maxim MAX658 @ 250 mA	15
V _{CC} Characteristics	1	5.2 Linear Tech LT1110-5 @ 150 mA	16
V _{PP} Characteristics	1		
2.1 Supplies for Battery Powered Applications	2		
The Modular Solution	2	6.0 12V V_{PP} SOLUTIONS: DOWN-CONVERTING FROM A HIGHER VOLTAGE	17
The Discrete Switching Regulator Solution	2	6.1 Maxim MAX667	18
Attributes of a DC-DC Converter	3	6.2 Linear Technology LT1111-5	19
3.0 12V V_{PP} SOLUTIONS: CONVERTING UP FROM 5V	3	6.3 National Semiconductor LM2940CT-12	20
3.1 Maxim MAX732	3		
3.2 Linear Technology LT1110-12	5		
3.3 Linear Technology LT1109-12	6		
3.4 Motorola MC34063A	8		
4.0 12V V_{PP} SOLUTIONS: CONVERTING UP FROM 3V	9		
4.1 Linear Technology LT1110-12	10		
4.2 Maxim MAX732 @ 30 mA	11		
4.3 Maxim MAX732 @ 60 mA	13		
		7.0 12V V_{PP} FROM 12V UNREGULATED	21
		8.0 SUMMARY	21
		APPENDIX A: Modular Solutions	A-1
		APPENDIX B: Survey of Solutions Presented	B-1
		APPENDIX C: Sources for DC-DC Converters	C-1
		APPENDIX D: Sources for Discrete Components	D-1
		APPENDIX E: Other Design Considerations	E-1
		APPENDIX F: PC Layouts	F-1

1.0 INTRODUCTION

Intel flash memory is rapidly being incorporated into a wide range of applications, adding enhanced capability to existing "traditional" memory markets, and creating new markets that exploit its benefits. Sometimes the design platforms may not possess the low powered 12V supply for writing flash memory. The system design engineer then needs to identify a power conversion solution with features and capabilities matching the needs of the application. For example, portable equipment requires a power supply converter that minimizes size and weight, maximizes efficiency to extend battery life, and can be switched into a standby mode to conserve power.

The following pages present some state of the art DC-DC converter solutions. These new solutions are smaller and more efficient than those typically seen in the past. Each of these solutions optimizes a subset of all possible power converter features. The choice of an optimal solution for a given application will be a tradeoff between several attributes. The solutions shown should meet the conversion needs of the majority of applications involving flash memory. Specifically, the solutions that follow encompass the following five categories:

- 5V to 12V conversion
- 3V (2 alkaline/NiCd cells) to 12V conversion
- 3V (2 Alkaline/NiCd cells) to 5V conversion
- Downconverting to 12V from a higher voltage
- Converting 12V unregulated to 12V regulated

More than one solution is presented within each of these categories. These different solutions have distinct optimal features/advantages. The optimal attributes of each solution are outlined. In addition, the appendix contains a survey of all solutions presented here, and provides a basis for comparing their features. The reader should reference it to choose an optimal solution for his/her application.

NOTE:

Solutions were selected from products offered by over thirty DC-DC converter vendors. Since this industry develops many new solutions each year, Intel recommends that designers contact vendors for latest products. Intel will continue to work with the industry to develop optimum solutions for power conversion. Intel Corporation assumes no responsibility for circuitry other than circuitry embodied in Intel products. No other circuit patent licenses are implied.

2.0 INTEL FLASH MEMORY POWER REQUIREMENTS

Intel flash memory is powered by two sources; a 5V V_{CC} line and a 12V V_{PP} line. V_{CC} is the primary power source and the only power source needed to read the memory. V_{PP} is required when writing or erasing the memory.

V_{CC} Characteristics

V_{CC} supplies power to the flash device during all operational modes. Maximum V_{CC} current is demanded by the device during the read operation. The data sheets for all Intel flash memory devices at the time this application note was written specify a maximum read current (I_{CC}) of 30 mA at 5V \pm 10%. This is the guaranteed worst case DC V_{CC} current that may be required by a flash device for reading one byte of data. If multiple components are read simultaneously, the V_{CC} current requirement increases proportionately. V_{CC} tolerance must be maintained to within specification limits at all times for proper functioning of the device.

V_{PP} Characteristics

The supplemental V_{PP} source provides the higher voltages needed to carry out the erase, erase verify, program, and program verify operations. Maximum V_{PP} current is typically demanded during the program and erase modes. Data sheets for all Intel flash memory devices at the time this application note was written specify a maximum I_{PP} current of 30 mA at 12V \pm 5% for both program and erase operations. This is the guaranteed worst case V_{PP} supply current that will be required by a flash device for writing one byte of data or erasing one block/component. If multiple components are programmed/erased simultaneously, the current requirement increases proportionately. V_{PP} must be maintained to within specification limits at all times during device program, and erase. The tolerance specification on V_{PP} must be strictly maintained. Over-voltage can damage the device, and under-voltage can decrease specified device reliability. Although the 12V supply must meet these worst case specifications, power usage will typically be much lower. The lower typical values seen in the data sheets should be used in calculating typical battery life.

2.1 Supplies for Battery Powered Applications

In applications where batteries are the primary source of power, the power supplies providing V_{CC} and V_{PP} need to be selected very carefully. Optimized operating efficiency of these supplies is important to extend battery life. Another attractive feature is the capability of these supplies to be switched into a very low power shutdown mode. It is important to minimize this shutdown current consumption as well since flash memory V_{PP} generators will often be in this state for extended periods of time. Moreover, since these supplies are used in equipment that is physically small and space-constrained, size and height of the supply need to be minimized.

Where two alkaline/NiCd batteries are used as the primary source of power, the primary voltage varies depending on the type and the state of discharge of the batteries. For example, alkaline batteries start life off at 1.5V, but may still retain a significant amount of energy when the voltage falls to 1.0V with use, and will work all the way down to 0.8V. On the other hand, NiCd cells maintain a near constant voltage of 1.25V throughout most of their discharge cycle, and work down to 1.0V. A solution that derives V_{CC} or V_{PP} from 2 AA batteries must hence be capable of doing so from an input voltage that lies in the range of 1.6V to 3.0V.

It is best to directly convert the primary battery voltage into the various voltages needed throughout the system. A step conversion (e.g. a 3V to 5V converter for V_{CC} , followed by a 5V to 12V converter for V_{PP}) is not recommended, since the inefficiency involved in each conversion step combines into one large inefficiency for the sum 3V to 12V conversion. Section 4 presents appropriate 3V battery to 12V converter solutions. Most of the solutions presented in this application note, while specifically designed for battery powered applications, are also viewed as ideal for other applications that incorporate flash memory.

2.2 Choice of a DC-DC Converter

The solution to finding the right power supply for flash memory lies in picking the right DC-DC converter for the job. Two broad categories of DC-DC converters available in the market today can be applied towards this purpose. These are the low power hybrid DC-DC converter module (or modular solution), and the low power discrete switching regulator IC solution.

The Modular Solution

The modular solution generally consists of a push-pull (Royer type) oscillator built around an isolation transformer, and in some cases followed by a linear regulator; all of which is encapsulated within a module. This hybrid module includes all components that are required by the DC-DC converter, and so no additional design effort is needed. The input and output voltages are fixed, and the input and output are almost always isolated via the isolation transformer. The main advantage of these solutions is that no design effort and/or external components are involved. They simply plug into a socket on a PC board. Disadvantages include lower efficiency (generally 60%), larger size/height (in most cases), and higher cost (generally 3x to 10x the cost of discrete solutions).

It would seem that the integration inherent in these solutions contributes towards system reliability, however the type and quality of the discrete components used internal to these hybrid devices is open to question. The isolation offered between the input and output is viewed as overkill for flash applications, since the total power required is typically less than 1W. Note also that the isolation transformer is often the main reason for the lower efficiencies.

The Discrete Switching Regulator Solution

The discrete switching regulator IC solution consists of a DC-DC converter IC (containing a switching regulator controller and an output power switch), along with a few discrete external components (inductor, diode, capacitors, resistors, etc.). The layout of the power supply system in this case is mostly left up to the user. However, application notes and data sheets explain the design process, and provide recommended circuits for commonly used solutions. The design can be tailored to deliver different output voltages and current levels depending on the characteristics of the input voltage and the external components.

Some vendors offer fixed output voltage versions, further simplifying the design process. The newer generation of high frequency low power switching regulator ICs are specifically targeted at battery powered operation, and most can be switched into a low quiescent current shutdown mode to extend battery life. These have typical efficiencies in the 75% to 90% range. Furthermore, the higher switching frequencies of these new parts (typically 100 KHz to 200 KHz) allow the use of smaller external components, which are available in surface mount varieties. As a consequence, these newer solutions are overall much smaller than what was typically seen just a year ago.

Attributes of a DC-DC Converter

Several attributes of a power supply converter must be evaluated and prioritized when choosing the best solution for a given application. These attributes include:

- Input Voltage Range
- Output Voltage and Tolerance
- Output Current Capability
- Efficiency of Conversion
- Printed Circuit Area
- Height
- Total Cost
- Shutdown Capability
- Quiescent Current Consumed in Shutdown Mode
- Rise Time from Shutdown
- Surface Mountability

The reader is referred to Appendix B, which provides a survey of all the solutions that are presented in this application note, in order to compare their attributes.

This application note primarily presents state of the art discrete switching regulator IC solutions which have been carefully designed for operation with flash memory. Included along with schematics are component values and sources/contacts for obtaining all the components. Actual layouts have also been included where possible. These are provided in Appendix F.

NOTE:

External components recommended in the designs should be used. These components (inductors, capacitors, resistors) were chosen based on recommendations by the converter IC vendors and provide the necessary quality for a clean design. Alternate "equivalent" parts should be chosen with care as their resistive and inductive elements can affect the operation of the solution. Please contact the respective converter IC companies for assistance if you select an alternate value/source for passive components.

3.0 V_{PP} SOLUTIONS: CONVERTING UP FROM 5V

Most computer systems have available a 5V V_{CC} line that is used for the majority of system power. Frequently, this 5V supply is used to generate 12V for flash memory. This section presents some of the new state of the art solutions that can achieve this function. These are all discrete switching regulators that optimize different attributes, mentioned along with the main features section of each example. Refer to Appendix B for a more detailed comparison of the attributes of these solutions.

3.1 Maxim Integrated Products—MAX732: V_{PP} @ 30 mA, 60 mA, 120 mA

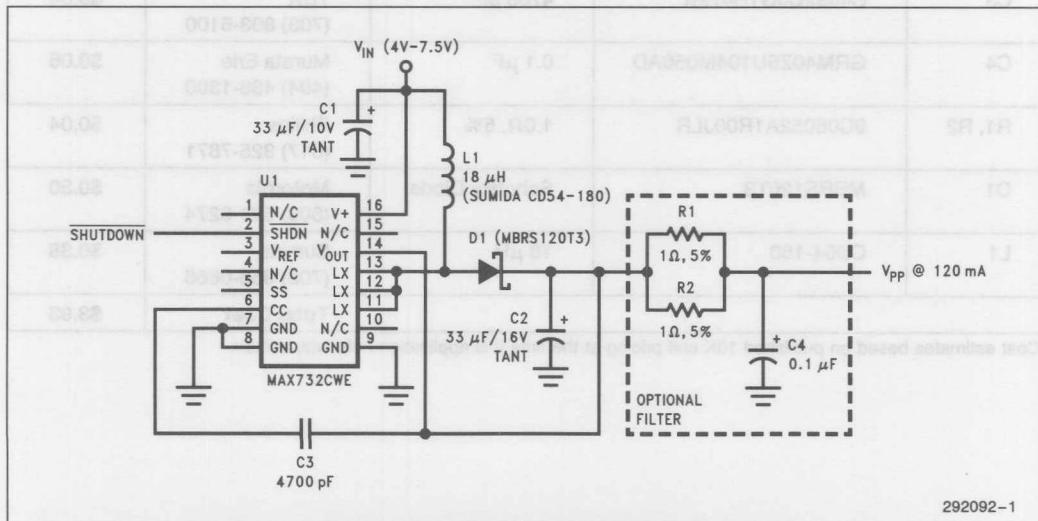


Figure 3-1. Maxim MAX732 5V to 12V Converter

Optimal Attributes

- Highest Efficiency
- Low Shutdown Current
- Wide Input Voltage Range
- All Surface Mount

Main Features

- Input Voltage Range: 4V to 7.5V
- Output Voltage: 12V $\pm 4\%$
- Output Current Capability: Up to 120 mA
- Typical Efficiency: 90% at $I_{LOAD} = 60$ mA
- 170 KHz Operation
- Shutdown Feature On Chip
- Low Quiescent Current at Shutdown: 70 μ A typical
- Low Operating Quiescent Current: 1.6 mA typical
- Rise Time from Shutdown: 1 ms Typical
- Will Work off Existing 5V Supply or a 6 NiCd Battery Pack

The MAX732 design as shown is capable of providing up to 120 mA of V_{PP} current at an efficiency of 90%. The 5V input should be able to source the peak currents and start-up currents required by the circuit. This converter circuit can also run directly off a 6 cell NiCd pack present on many notebook/laptop computers. It is available in a 16-pin wide SOIC package, and uses small external surface mount components (5 in all). Voltage spikes may be present in the output due to incorrect layout, excessive output filter capacitor ESL (Equivalent Series Inductance) and diode switching transients. The optional filter circuit is recommended to eliminate any sharp transients. The supply can be switched into a shutdown mode where the output voltage falls to approximately V_{CC} - 550 mV. A layout is presented in Appendix F. Applications assistance and a surface mount evaluation kit is also available from Maxim.

Table 3-1. Parts List for the MAX732 5V to 12V Converter

Ref	Part #	Value/Type	Source	Cost*
U1	MAX732CWE	SMPS IC	Maxim (408) 737-7600	\$2.50
C1	267M1002-336-MR-720	33 μ F/10V Tantalum	Matsuo (714) 969-2491	\$0.31
C2	267M1602-336-MR-720	33 μ F/16V Tantalum	Matsuo (714) 969-2491	\$0.31
C3	C4532C0G1H472K	4700 pF	TDK (708) 803-6100	\$0.04
C4	GRM40Z5U104M050AD	0.1 μ F	Murata Erie (404) 436-1300	\$0.06
R1, R2	9C08052A1R00JLR	1.0 Ω , 5%	Philips (817) 325-7871	\$0.04
D1	MBRS120T3	Schottky Diode	Motorola (800) 521-6274	\$0.30
L1	CD54-180	18 μ H	Sumida (708) 956-0666	\$0.38
Total Cost				\$3.93

*Cost estimates based on published 10K unit pricing at the time this application note was written.

3.2 Linear Technology LT1110-12: V_{PP} @ 30 mA, 60 mA, 120 mA

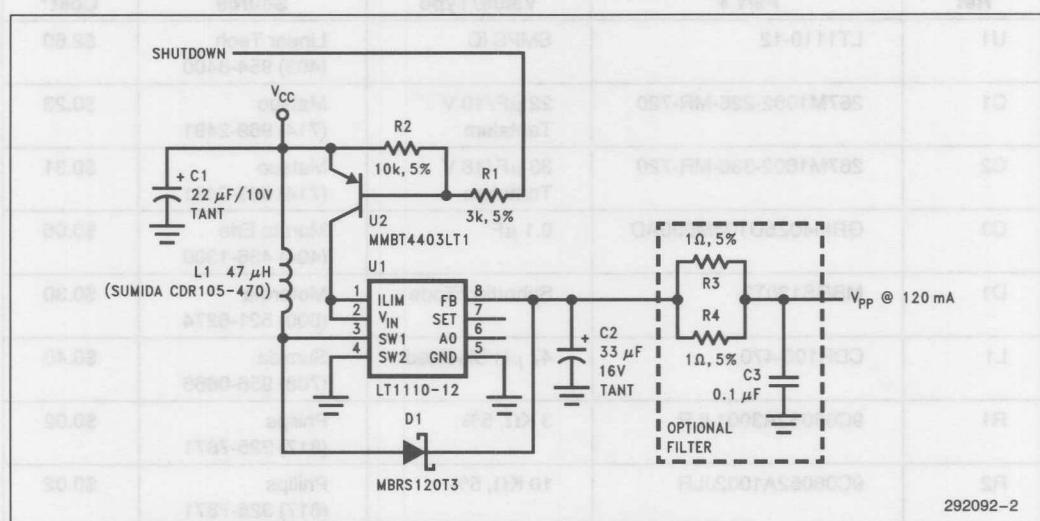


Figure 3-2. Linear Technology LT1110-12 5V to 12V Converter

Optimal Attributes

- Small Size: 0.45 sq. in. Total Board Area (Single Sided)
- Very Low Shutdown Current: 16 μ A
- All Surface Mount

Main Features

- Input Voltage Range: 4.5V to 5.5V
- Output Voltage: 12V \pm 5%
- Output Current Capability: Up to 120 mA
- Typical Efficiency: 76%
- 60 KHz Operation
- Shutdown Possible Using External Components as Shown
- Low Quiescent Current at Shutdown: 16 μ A typical
- Rise Time from shutdown: 800 μ s typical

The Linear Technology LT1110-12 is a fixed 12V output part which is well suited to flash memory applications. The part is available in a small 8-pin surface mount (SO8) package. The part needs 7 external components to implement a small size 5V to 12V converter solution that can be shutdown to a very low quiescent current state—16 μ A typical. The 5V source must be capable of supplying the instantaneous start-up and peak currents required during operation. Voltage spikes may be present in the output due to incorrect layout, excessive output filter capacitor ESL (Equivalent Series Inductance) and diode switching transients. The optional RC filter circuit is recommended in order to eliminate these sharp transients. The output voltage during shutdown falls to approximately $V_{IN} - 550$ mV. A recommended board layout appears in Appendix F. Applications assistance is available from Linear Technology Corporation.



Table 3-2. Part List for the LT1110-12 5V to 12V Converter

Ref	Part #	Value/Type	Source	Cost*
U1	LT1110-12	SMPS IC	Linear Tech (408) 954-8400	\$2.60
C1	267M1002-226-MR-720	22 μ F/10 V Tantalum	Matsuo (714) 969-2491	\$0.23
C2	267M1602-336-MR-720	33 μ F/16 V Tantalum	Matsuo (714) 969-2491	\$0.31
C3	GRM40Z5U104M050AD	0.1 μ F	Murata Erie (404) 436-1300	\$0.06
D1	MBRS120T3	Schottky Diode	Motorola (800) 521-6274	\$0.30
L1	CDR105-470	47 μ H Shielded	Sumida (708) 956-0666	\$0.40
R1	9C08052A3001JLR	3 K Ω , 5%	Philips (817) 325-7871	\$0.02
R2	9C08052A1002JLR	10 K Ω , 5%	Philips (817) 325-7871	\$0.02
R3, R4	9C08052A1R00JLR	1 Ω , 5%	Philips (817) 325-7871	\$0.04
U2	MMBT4403LT1	2N4403 PNP Transistor	Motorola (800) 521-6274	\$0.09
Total Cost				\$4.07

*Cost estimates based on published 10K unit pricing at the time this application note was written.

3.3 Linear Technology LT1109-12: V_{PP} @ 30 mA, 60 mA

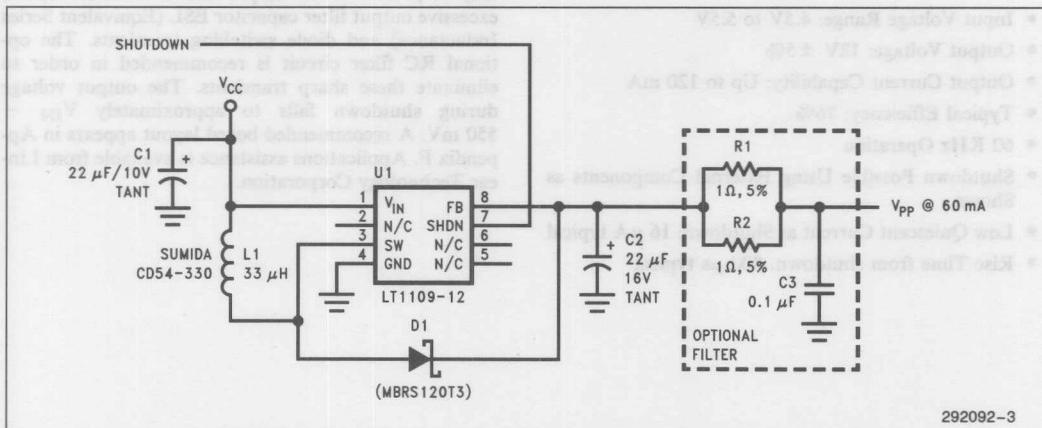


Figure 3-3. Linear Technology LT1109-12 5V to 12V Converter

Optimal Attributes

- Smallest Size
- Low Shutdown Current
- All Surface Mount

Main Features

- Input Voltage Range: 4.5V to 5.5V
- Output Voltage: 12V $\pm 5\%$
- Output Current Capability: Up to 60 mA
- Typical Efficiency: 84%
- 130 KHz Operation
- Shutdown Feature On Chip
- Low Quiescent Current at Shutdown: 375 μ A typical
- Rise Time from shutdown: 800 μ s typical
- Small Size: SO8 plus 4 small external components

The Linear Technology LT1109-12 is a fixed 12V output part which is very well suited to flash memory applications. The part is available in a very small 8-pin surface mount (SO8) package. The part needs just 4 small external components to implement an extremely small size 5V to 12V converter solution that can be shutdown to a low quiescent current state—375 μ A typical. The 5V source must be capable of supplying the instantaneous start-up and peak currents required by the operation. Voltage spikes may be present in the output due to incorrect layout, excessive output filter capacitor ESL (Equivalent Series Inductance) and diode switching transients. The optional RC filter circuit is recommended in order to eliminate these sharp transients. The output during shutdown falls to approximately $V_{IN} - 550$ mV. A typical board layout is presented in Appendix F. Applications assistance is available from Linear Technology Corporation.

Table 3-3. Parts List for the LT1109-12 5V to 12V Converter

Ref	Part #	Value/Type	Source	Cost*
U1	LT1109-12	SMPS IC	Linear Tech (408) 432-1900	\$2.37
C1	267M1002-226-MR-720	22 μ F/10V Tant Chip Capacitor	Matsuo (714) 969-2491	\$0.23
C2	267M2502-106-MR-720	10 μ F/25V Tant Chip Capacitor	Matsuo (714) 969-2491	\$0.29
C3	GRM40Z5U104M050AD	0.1 μ F	Murata Erie (404) 436-1300	\$0.06
D1	MBRS120T3	Schottky Diode	Motorola (800) 521-6274	\$0.30
R1, R2	9C08052A1R00JLR	1 Ω , 5%	Philips (817) 325-7871	\$0.04
L1	CD54-330	33 μ H	Sumida (708) 956-0666	\$0.32
Total Cost				\$3.61

*Cost estimates based on published 10K unit pricing at the time this application note was written.

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3.4 Motorola MC34063A: V_{PP} @ 30 mA, 60 mA, 120 mA

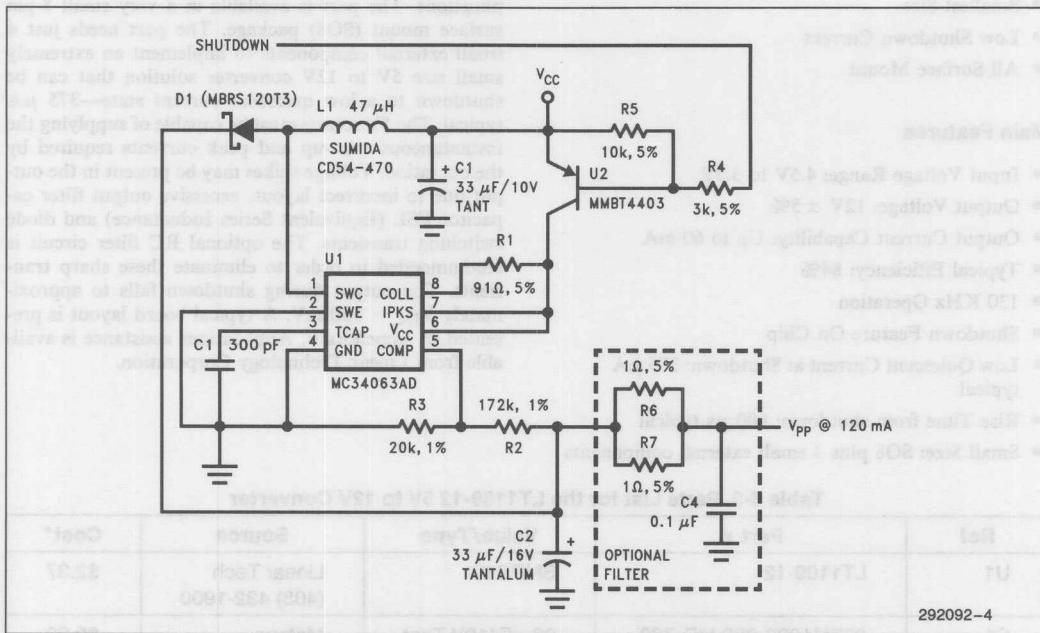


Figure 3-4. Motorola MC34063A 5V to 12V Converter

Optimal Attributes

- Lowest Cost
- Very Low Shutdown Current
- All Surface Mount

Main Features

- Input Voltage Range: 4.5V to 5.5V
- Output Voltage: 12V ± 5%
- Output Current Capability: Up to 120 mA
- Typical Efficiency: 80%
- 100 KHz Operation
- Shutdown Feature Using External Components
- Low Quiescent Current at Shutdown: 25 μA typical
- Rise Time From Shutdown: 2 ms typical
- SO8 Plus 11 Small External Components—All SMD

The Motorola MC34063A solution presented uses 11 small sized external components to implement a low cost surface mount 5V to 12V converter solution. Three external components (U2, R4, R5) are used to shut down supply to the part when V_{PP} is not needed. These could be eliminated to further lower the cost if power consumption is not important. The quiescent current in shutdown state is a low 25 μA. The output voltage in shutdown is V_{CC} – 550 mV. Voltage spikes may be present in the output due to incorrect layout, excessive output filter capacitor ESL (Equivalent Series Inductance) and diode switching transients. The optional RC filter circuit is recommended in order to eliminate these sharp transients. Applications assistance is available from Motorola.

Table 3-4. Parts List for the MC34063A 5V to 12V Converter

Ref	Part #	Value/Type	Source	Cost*
U1	MC34063AD	SMPS IC (SO8)	Motorola (800) 521-6274	\$0.63
R1	9C08052A9100JLR	91Ω, 5%	(Philips (817) 325-7871	\$0.02
R2	9B08053A1723FCB	172 KΩ, 1%	(Philips (817) 325-7871	\$0.04
R3	9B08053A2002FCB	20 KΩ, 1%	Philips (817) 325-7871	\$0.04
R4	9C08052A3001JLR	3 KΩ, 5%	Philips (817) 325-7871	\$0.02
R5	9C08052A1002JLR	10 KΩ, 5%	Philips (817) 325-7871	\$0.02
R6, R7	9C08052A1R00JLR	1Ω, 5%	Philips (817) 325-7871	\$0.04
C1	267M1002-336-MR-720	33 µF/16V Tantalum	Matsuo (714) 969-2491	\$0.28
C2	267M1602-336-MR-720	33 µF/16V Tantalum	Matsuo (714) 969-2491	\$0.31
C3	GRM40X7R301M050AD	300 pF	Murata Erie (404) 436-1300	\$0.03
C4	GRM40Z5U104M050AD	0.1 µF	Murata Erie (404) 436-1300	\$0.06
D1	MBRS120T3	Schottky Diode	Motorola (800) 521-6274	\$0.30
L1	CD54-470	47 µH	Sumida (708) 956-0666	\$0.37
U2	MMBT4403LT1	PNP Transistor	Motorola (800) 521-6274	\$0.09
Total Cost				\$2.25

* Cost estimates based on published 10K unit pricing at the time this application note was written.

4.0 **V_{PP} SOLUTIONS: CONVERTING UP FROM 2 NiCd/ALKALINE CELLS**

Palmtop computers that use 2 alkaline/NiCd batteries require that the system work even when the battery

voltage is down near 1.8V. Currently there exist two good solutions that achieve a 12V output with inputs as low as 1.8V, and yet supply at least 30 mA of current. These are the LT1110-12 from Linear Technology Corporation, and the MAX732 from Maxim Integrated Products.

4.1 Linear Technology LT1110-12: V_{PP} @ 30 mA from 2 AA Cells

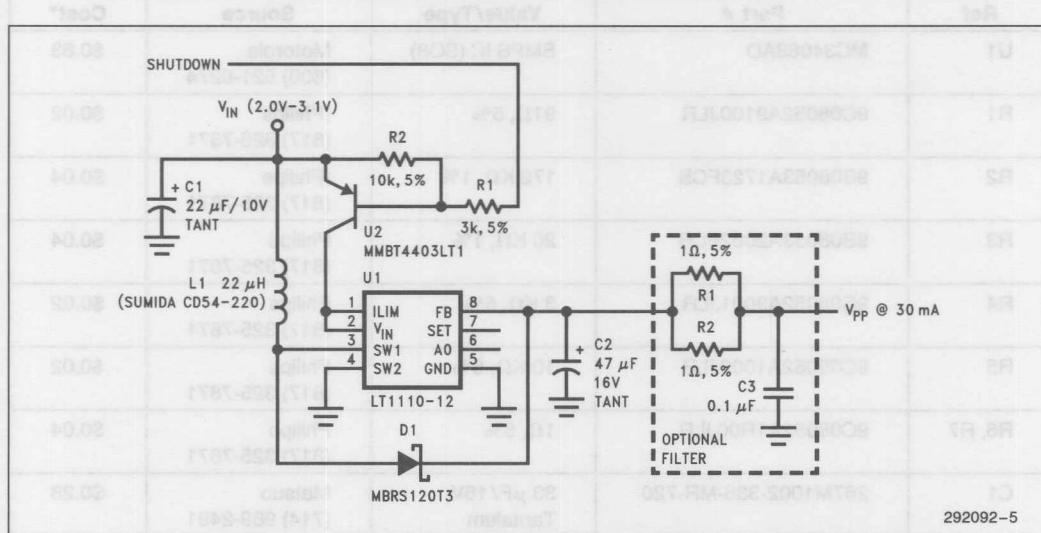


Figure 4-1. Linear Technology LT1110-12 3V to 12V Converter

Optimal Attributes

- Smallest Size
 - Low Shutdown Current
 - All Surface Mount

Main Features

- Input Voltage Range: 2.0V to 3.1V
 - Output Voltage: 12V \pm 5%
 - Output Current Capability: Up to 30 mA
 - Typical Efficiency: 70%
 - 60 KHz Operation
 - Shutdown Mode Using External Components
 - Low Quiescent Current at Shutdown: 16 μ A typical
 - Rise Time from Shutdown: 4 ms typical

The LT1110-12 from Linear Technology Corporation, as shown, can be used to generate V_{PP} from an input voltage between 2.0V and 3.1V (most of the usable life of 2 alkaline/NiCd cells in series). This design is similar to the 5V to 12V converter design presented in Section 3.2. Replacing L1 and C2 with a lower inductance and a higher capacitance, respectively, allows the part to work down to 2.0V, while reducing the output current capability to 30 mA. The external PNP transistor is used to shut off the input supply to the converter IC, and puts the part in shutdown state. Note that a disadvantage of this scheme of shutdown is that the control signal source sinks approximately 5 mA ($V_{CC}/1K$) when the part is not in shutdown. However, the quiescent current in shutdown state is a low 16 μA . See Appendix E for an alternate shutdown solution. The output voltage in shutdown falls to approximately $V_{IN} - 550$ mV. Voltage spikes may be present in the output due to incorrect layout, excessive output filter capacitor ESL (Equivalent Series Inductance) and diode switching transients. The optional RC filter circuit is recommended in order to eliminate any sharp transients. A surface mount layout appears in Appendix F.

Table 4-1. Parts List for the LT1110-12 3V to 12V Converter

Ref	Part #	Value/Type	Source	Cost*
U1	LT1110-12	SMPS IC	Linear Tech (408) 954-8400	\$2.60
C1	267M1002-220-MR-720	22 µF/10V Tantalum	Matsuo (714) 969-2491	\$0.23
C2	267M1602-470-MR-720	47 µF/16V Tantalum	Matsuo (714) 969-2491	\$0.47
C3	GRM40Z5U104M050AD	0.1 µF	Murata Erie (404) 436-1300	\$0.06
D1	MBRS120T3	Schottky Diode	Motorola (800) 521-6274	\$0.30
L1	CD54-220	22 µH	Sumida (708) 956-0666	\$0.37
R1	9C08052A3001JLR	3 KΩ, 5%	Philips (817) 325-7871	\$0.02
R2	9C08052A1002JLR	10 KΩ, 5%	Philips (817) 325-7871	\$0.02
R3, R4	9C08052A1R00JLR	1Ω, 5%	Philips (817) 325-7871	\$0.04
U2	MMBT4403LT1	2N4403 PNP Transistor	Motorola (800) 521-6274	\$0.09
Total Cost				\$4.20

*Cost estimates based on published 10K unit pricing at the time this application note was written.

4.2 Maxim Integrated Products—MAX732: V_{PP} @ 30 mA

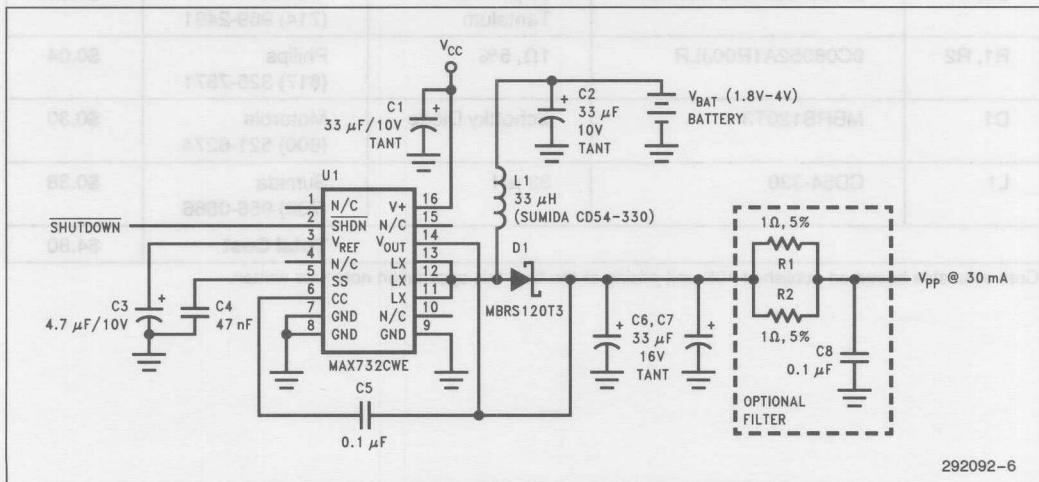


Figure 4-2. Maxim MAX732 3V to 12V Converter (30 mA)

Optimal Attributes

- Highest Efficiency
- All Surface Mount

Main Features

- Input Voltage Range: 1.8V to 5.0V
- Output Voltage: 12V $\pm 4\%$
- Output Current Capability: Up to 30 mA
- Typical Efficiency: 87%
- 170 KHz Operation
- Shutdown Mode On Chip
- Low Quiescent Current at Shutdown: 45 μ A typical
- Rise Time from shutdown: 25 ms typical

The MAX732 circuit as shown here can provide up to 30 mA at 12V from an input voltage as low as 1.8V. Note that the chip itself is powered from the 5V V_{CC} line required to use present day flash memory devices, whereas the inductor is connected to the primary battery supply. Voltage spikes may be present in the output due to incorrect layout, excessive output filter capacitor ESL and diode switching transients. The optional RC filter circuit is recommended in order to eliminate these sharp transients. Applications assistance and an evaluation kit is available from Maxim.

Table 4-2. Parts List for the MAX732 3V to 12V Converter (30 mA)

Ref	Part #	Value/Type	Source	Cost*
U1	MAX732CWE	SMPS IC	Maxim (408) 737-7600	\$2.50
C1, C2	267M1002-336-MR-720	33 μ F/10V Tantalum	Matsuo (714) 969-2491	\$0.56
C3	267M1002-475-MR-720	4.7 μ F/10V Tantalum	Matsuo (714) 969-2491	\$0.20
C4	GRM40X7R473M050AD	47 nF	Murata Erie (404) 436-1300	\$0.08
C5, C8	GRM40Z5U104M050AD	0.1 μ F	Murata Erie (404) 436-1300	\$0.12
C6, C7	267M1602-336-MR-720	33 μ F/16V Tantalum	Matsuo (714) 969-2491	\$0.62
R1, R2	9C08052A1R00JLR	1 Ω , 5%	Philips (817) 325-7871	\$0.04
D1	MBRS120T3	Schottky Diode	Motorola (800) 521-6274	\$0.30
L1	CD54-330	33 μ H	Sumida (708) 956-0666	\$0.38
Total Cost				\$4.80

*Cost estimates based on published 10K unit pricing at the time this application note was written.

4.3 Maxim Integrated Products—MAX732: V_{PP} @ 60 mA

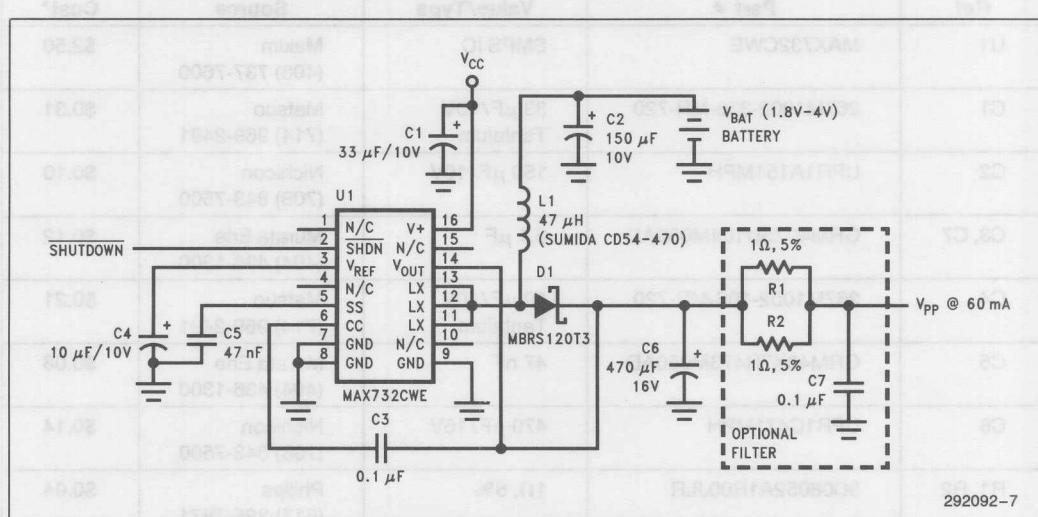


Figure 4-3. Maxim MAX732 3V to 12V Converter (60 mA)

Optimal Attributes

- Highest Efficiency
- 60 mA Output Current Capability

Main Features

- Input Voltage Range: 1.8V to 5.0V
- Output Voltage: 12V ±4%
- Output Current Capability: Up to 60 mA
- Typical Efficiency: 87%
- 170 KHz Operation
- Shutdown Mode On Chip
- Low Quiescent Current at Shutdown: 45 μA typical
- Rise Time from shutdown: 75 ms typical

The MAX732 circuit as shown here can provide up to 60 mA at 12V from an input voltage as low as 1.8V. This solution is similar to the previous one presented but is not entirely surface mountable, because of the larger output and input filter capacitors. Currently, it is the only solution employing a single IC that can provide 60 mA at 12V from a 1.8V input. The 470 μF/16V filter capacitor must be a low-ESR (Equivalent Series Resistance) type. Voltage spikes may be present in the output due to incorrect layout, excessive output filter capacitor ESL (Equivalent Series Inductance) and diode switching transients. The optional RC filter circuit is recommended in order to eliminate these sharp transients. Applications assistance and an evaluation kit is available from Maxim.

Table 4-3. Parts List for the MAX732 3V to 12V Converter (60 mA)

Ref	Part #	Value/Type	Source	Cost*
U1	MAX732CWE	SMPS IC	Maxim (408) 737-7600	\$2.50
C1	267M1002-336-MR-720	33 μ F/10V Tantalum	Matsuo (714) 969-2491	\$0.31
C2	UPR1A151MPH	150 μ F/10V	Nichicon (708) 843-7500	\$0.10
C3, C7	GRM40Z5U104M050AD	0.1 μ F	Murata Erie (404) 436-1300	\$0.12
C4	267M1002-106-MR-720	10 μ F/10V Tantalum	Matsuo (714) 969-2491	\$0.21
C5	GRM40X7R473M050AD	47 nF	Murata Erie (404) 436-1300	\$0.08
C6	UPR1C471MPH	470 μ F/16V	Nichicon (708) 843-7500	\$0.14
R1, R2	9C08052A1R00JLR	1 Ω , 5%	Philips (817) 325-7871	\$0.04
D1	MBRS120T3	Schottky Diode	Motorola (800) 521-6274	\$0.30
L1	CD75-470	47 μ H	Sumida (708) 956-0666	\$0.38
Total Cost				\$4.15

*Cost estimates based on published 10K unit pricing at the time this application note was written.

5.0 V_{CC} SOLUTIONS: CONVERTING UP FROM TWO NiCd/ALKALINE CELLS

Palmtop and hand-held computers that use two AA size NiCd or alkaline batteries need a converter solution.

tion to provide the V_{CC} supply for the system as well as flash memory. Two good solutions are offered currently for this purpose, the MAX658 from Maxim Integrated Products and the LT1110-5 from Linear Technology Corporation.

5.1 Maxim Integrated Products—MAX658: V_{CC} @ 250 mA

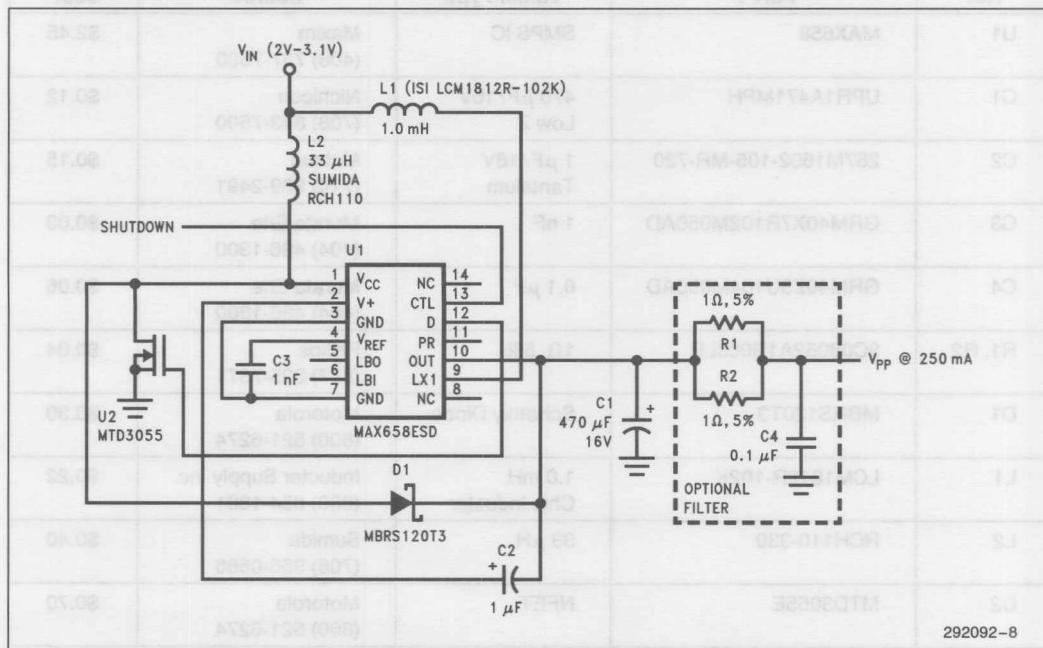


Figure 5-1. Maxim MAX658 3V to 5V Converter (250 mA)

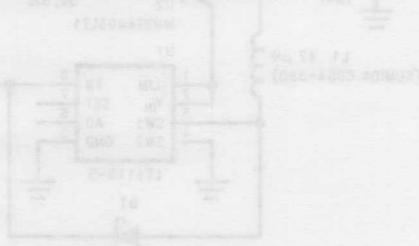
Optimal Attributes

- Highest Efficiency
- 250 mA Output Current Capability
- Low Shutdown Current

Main Features

- Input Voltage Range: 2.0V to 3.1V
- Output Voltage: 5V ± 10%
- Output Current Capability: Up to 250 mA
- Typical Efficiency: 85%
- 18 KHz Operation
- Shutdown Mode On Chip
- Low Quiescent Current at Shutdown: 80 μA typical
- Rise Time from shutdown: 25 ms typical

The MAX658, available from Maxim Integrated Products in a 14-pin surface mount package, is a good high current solution for obtaining V_{CC} from a pair of NiCd/alkaline cells. The entire solution, however, is not 100% surface mountable. It uses a high current through-hole inductor and a large through-hole filter capacitor at the output. Voltage spikes may be present in the output due to incorrect layout, excessive output filter capacitor ESR (Equivalent Series Resistance) and diode switching transients. The optional RC filter circuit is recommended in order to eliminate any sharp transients. Applications assistance and an evaluation kit are available from Maxim.



(An OSAT member of the QCAV2 of VQ-6011 TJ technology family)

Table 5-1. Parts List for the MAX658 3V to 5V Converter

Ref	Part #	Value/Type	Source	Cost*
U1	MAX658	SMPS IC	Maxim (408) 737-7600	\$2.45
C1	UPR1A471MPH	470 μ F/10V Low Z	Nichicon (708) 843-7500	\$0.12
C2	267M1602-105-MR-720	1 μ F/16V Tantalum	Matsuo (714) 969-2491	\$0.15
C3	GRM40X7R102M050AD	1 nF	Murata Erie (404) 436-1300	\$0.03
C4	GRM40Z5U104M050AD	0.1 μ F	Murata Erie (404) 436-1300	\$0.06
R1, R2	9C08052A1R00JLR	1 Ω , 5%	Philips (817) 325-7871	\$0.04
D1	MBRS120T3	Schottky Diode	Motorola (800) 521-6274	\$0.30
L1	LCM1812R-102K	1.0 mH Chip Inductor	Inductor Supply Inc. (800) 854-1881	\$0.22
L2	RCH110-330	33 μ H	Sumida (708) 956-0666	\$0.40
U2	MTD3055E	NFET	Motorola (800) 521-6274	\$0.70
Total Cost				\$4.47

*Cost estimates based on published 10K unit pricing at the time this application note was written.

5.2 Linear Technology LT1110-5: V_{CC} @ 150 mA

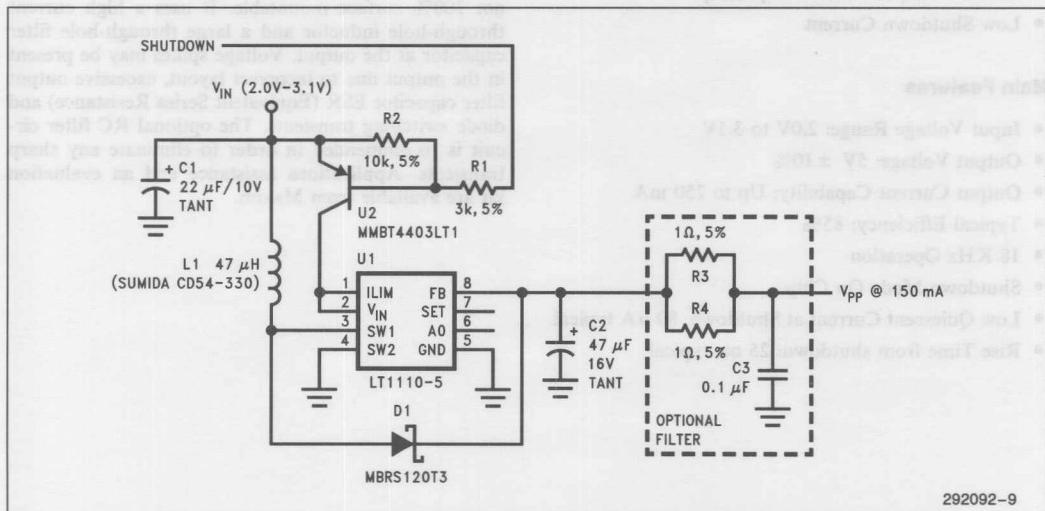


Figure 5-2. Linear Technology LT1110-5 3V to 5V Converter (150 mA)

Optimal Attributes

- Smallest Size
- Low Shutdown Current
- All Surface Mount

- Typical Efficiency: 76%
- 60 KHz Operation
- Shutdown Mode Using External Components
- Low Quiescent Current at Shutdown: 16 μ A typical
- Rise Time from Shutdown: 4 ms typical

Main Features

- Input Voltage Range: 2.0V to 3.1V
- Output Voltage: 5V \pm 5%
- Output Current Capability: Up to 150 mA

The LT1110-5 from Linear Technology is a fixed 5V version of the converter shown for the 12V design in Section 4.1.

Table 5-2. Parts List for the LT1110-5 3V to 5V Converter

Ref	Part #	Value/Type	Source	Cost*
U1	LT1110-5CS8	SMPS IC	Linear Tech (408) 954-8400	\$2.60
C1	267M1002- 226-MR-720	22 μ F/10V Tantalum Chip	Matsuo (714) 969-2491	\$0.23
C2	267M1602- 476-MR-720	47 μ F/16V Tantalum Chip	Matsuo (714) 969-2491	\$0.47
C3	GRM40Z5U104M050AD	0.1 μ F	Murata Erie (404) 436-1300	\$0.06
D1	MBRS120T3	Schottky Diode	Motorola (800) 521-6274	\$0.30
L1	CD75-330	33 μ H	Sumida (708) 956-0666	\$0.38
R1	9C08052A3001JLR	3 K Ω , 5%	Philips (817) 325-7871	\$0.02
R2	9C08052A1002JLR	10 K Ω , 5%	Philips (817) 325-7871	\$0.02
R3, R4	9C08052A1R00JLR	1 Ω , 5%	Philips (817) 325-7871	\$0.04
U2	MMBT4403LT1	PNP Transistor	Motorola (800) 521-6274	\$0.09
Total Cost				\$4.21

*Cost estimates based on published 10K unit pricing at the time this application note was written.

6.0 DOWN-CONVERTING TO 12V

The ability to down-convert to 12V from a higher voltage is often needed (as in the telecommunications environment). This section presents some good solutions for obtaining V_{PP} from a higher voltage.

6.1 Maxim Integrated Products MAX667

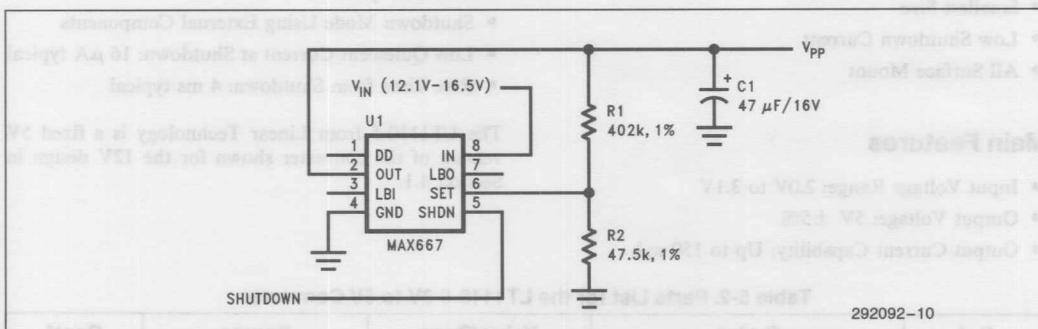


Figure 6-1. Maxim MAX667 12V Linear Voltage Regulator

Optimal Attributes

- Small Size
- Ultra Low Shutdown Current
- All Surface Mount
- Very Low Dropout
- Output Current Capability: Up to 120 mA
- Typical Efficiency: 70%
- Shutdown Mode On Chip
- Low Quiescent Current at Shutdown: 0.2 μ A Typical
- Rise Time from Shutdown: Less than 0.1 ms Typical

Main Features

- Input Voltage Range: 12.1V to 16.5V
- Output Voltage: 12V \pm 5%

Table 6-1. Parts List for the MAX667 12V Step Down Converter

Ref	Part #	Value/Type	Source	Cost*
U1	MAX667CSA	SMPS IC-SO8 Package	Maxim (408) 737-7600	\$2.10
C1	267M1602-476-MR-720	7 μ F/16V Tantalum	Matsuo (714) 969-2491	\$0.47
R1	9C08053A4023JLR	402 K Ω , 1%	Philips (817) 325-7871	\$0.03
R2	9C08053A4752JLR	47.5 K Ω , 1%	Philips	\$0.03
Total Cost				\$2.63

*Cost estimates based on published 10K unit pricing at the time this application note was written.

6.2 Linear Technology Corporation LT1111-12 Step Down Switcher

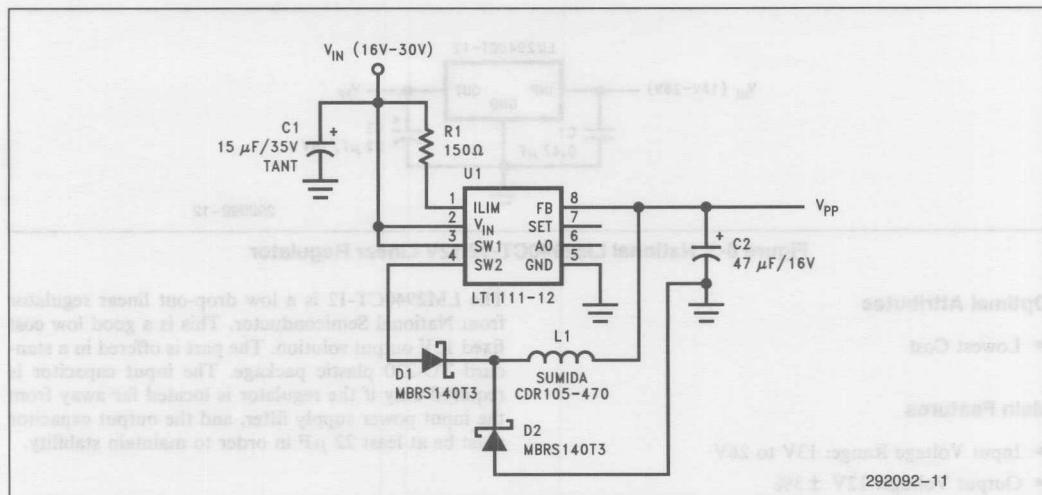


Figure 6-2. Linear Technology LT1111-12 Step Down Switcher

Optimal Attributes

- High Efficiency
- All Surface Mount

Main Features

- Input Voltage Range: 16V to 30V
- Output Voltage: 12V \pm 5%
- Output Current Capability: Up to 120 mA
- Typical Efficiency: 80%

Table 6-2. Parts List for the LT1111-12 12V Step Down Converter

Ref	Part #	Value/Type	Source	Cost*
U1	LT1111-12	SMPS IC-SO8 Package	Linear Tech (408) 432-1900	\$2.20
C1	267M3502-225-MR-720	2.2 μF/35V Tantalum	Matsuo (714) 969-2491	\$0.28
C2	267M1602-476-MR-720	47 μF/16V Tantalum	Matsuo (714) 969-2491	\$0.47
R1	9C08052A1500JLR	150Ω, 5%	Philips (817) 325-7871	\$0.02
L1	CDR105-470	47 μH	Sumida (708) 956-0666	\$0.38
D1, D2	MBRS140T3	Schottky Diode	Motorola (800) 521-6274	\$0.60
Total Cost				\$3.95

*Cost estimates based on published 10K unit pricing at the time this application note was written.

6.3 National Semiconductor LM2940CT-12

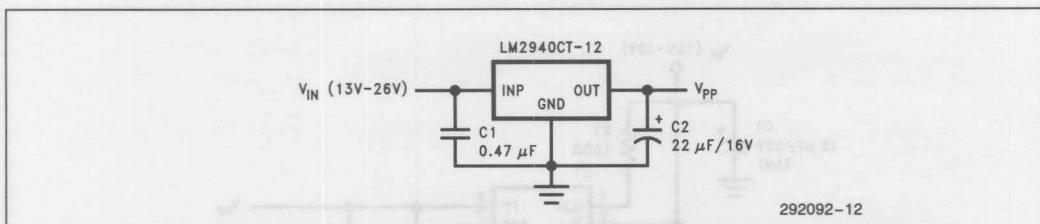


Figure 6-3. National LM2940CT-12 12V Linear Regulator

Optimal Attributes

- Lowest Cost

Main Features

- Input Voltage Range: 13V to 26V
- Output Voltage: 12V \pm 3%
- Output Current Capability: 1A

The LM2940CT-12 is a low drop-out linear regulator from National Semiconductor. This is a good low cost fixed 12V output solution. The part is offered in a standard TO-220 plastic package. The input capacitor is required only if the regulator is located far away from the input power supply filter, and the output capacitor must be at least 22 μ F in order to maintain stability.

Table 6-3. Parts List for the LM2940CT-12 Step Down Converter

Ref	Part #	Value/Type	Source	Cost*
U1	LM2940CT-12	Voltage Reg TO-220	National (408) 721-5000	\$0.95
C1	GRM43-2Z5U474M050AD	0.47 μ F/50V	Murata Erie (404) 436-1300	\$0.07
C2	267M1602-226-MR-720	22 μ F/16V Tantalum	Matsuo (714) 969-2491	\$0.28
Total Cost				\$1.30

*Cost estimates based on published 10K unit pricing at the time this application note was written.

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00.00	00.00	00.00	00.00	00.00

7.0 OBTAINING V_{PP} FROM 12V UNREGULATED

In systems like the desktop computer, a 12V supply exists but may not be regulated to $\pm 5\%$. If this voltage is used as the V_{PP} source for flash memory, it may well degrade the write/erase performance of the memory, or adversely affect its reliability. Fortunately, in most of the situations where a 12V unregulated (or not regulated to within 5%) supply exists, a 5V supply also exists in the system (the desktop computer is a good example). It is recommended in such cases that the existing 5V supply be used to obtain the 12V $\pm 5\%$ rail. This approach is more economical, more efficient, and provides space savings over a buck-boost topology that takes unregulated 12V and regulates it to $\pm 5\%$.

In the rare case where a 5V supply is not present, modular solutions exist that will regulate the unregulated 12V supply to $\pm 5\%$. However, these are bulky and expensive. Moreover, many of them require that a minimum load be maintained in order to stay in regulation. One such solution is presented in Appendix A.

8.0 SUMMARY

For battery powered applications, the author views the discrete switching regulator IC solution as a better choice than the modular solution. The lower cost, higher efficiency, and smaller size/height associated with discrete solutions justify the small additional design effort required to incorporate them in flash memory applications. In applications where the primary source of power is a wall power outlet, or in applications where the flash memory will be written to infrequently, efficiency and quiescent current take on secondary importance. In such cases, it may be acceptable to use a 12V regulated (to within $\pm 5\%$) tap from the system supply. Alternatively, the ability to easily design-in modular solutions may outweigh the disadvantages of lower efficiency and increased cost. For those users wishing to incorporate modular solutions, Appendix A provides some of the lower cost solutions from this industry segment.

APPENDIX A MODULAR SOLUTIONS

Modular solutions may work well in non-battery powered situations where the efficiency of the power supply converter is not critical. These are also advantageous in that they usually do not need any external components and there is no converter design involved. However, the type and quality of the discrete components used in these hybrid solutions is open to question. This is not true in the case of the discrete converter designs presented in the earlier sections, where the quality of the components used are under the control of the system design engineer. Hence, even though modular solutions offer the convenience of a single package and ease of testability, the quality/reliability of comparably priced modular solutions may be questionable.

Some modular solutions suited to flash memory applications are presented below, with a brief description of each. Sources for obtaining these are listed in Appendix B.

A.1 International Power/Newport Components NMF0512S

The NMF0512S is a 5V to 12V hybrid power module that has an output current capability of 80 mA. Output tolerance is $\pm 5\%$. It is equipped with a shutdown pin which can be used to switch V_{pp} off. However, power dissipated in the shutdown mode is relatively high (about 100 mW). The part is small in size and measures 0.76 in. (19.5 mm) x 0.4 in. (9.8 mm) x 0.4 in. (9.8 mm), and costs about \$7.90 in 10K quantities (at the time this application note was written). Typical efficiency of conversion is 62%.

A.2 Xentek NPSC-0512S

The Xentek NPSC-0512S is a 1W power module that converts 5V to V_{pp} and will source up to 80 mA of continuous current. However, it uses two external filter capacitors—one at the input and one at the output. The input filter capacitor is 47 μ F/10V, and the output filter capacitor is 100 μ F/16V. Size of the solution (converter alone) is 0.87 in. (22 mm) x 0.39 in. (10 mm) x 0.79 in. (20 mm). The NPSC-0512S does not have a shutdown mode. The part costs around \$5.00 in 10K quantities (at the time this application note was written). Typical efficiency of conversion is 60%.

A.3 Shindengen America Inc. HDF-0512D

The HDF-0512D module from Shindengen will convert unregulated 12V to 12V $\pm 5\%$. This part is a dual output part ($\pm 12V$), but only the +12V line is used. The conversion efficiency is high (75% typical), and the part will provide a regulated V_{pp} voltage from input voltages as low as 8V, and as high as 16.5V. A minimum load of 5 mA needs to be maintained to guarantee regulation. Size of the solution is 1.75 in. (44 mm) x 0.43 in. (11 mm) x 0.8 in. (20 mm). Cost is approximately \$10.00 in quantities of 10K (at the time this application note was written).

APPENDIX B SURVEY OF SOLUTIONS PRESENTED

B-1

Ref #	Vendor Name	Part #	Input C (Volts)	Output V (Volts)	Output C (mA)	Effic (%)	# Ext Comp (Note 1)	100% SMD ?	Cost (Note 2)	PC Area (Note 3)	Height (In)	SHDN ?	ISHDN (Note 4)	R Time (Note 5)	Temp
3.1	Maxim	MAX732	4V–7V	12V, 4%	120	90	5; D, L, 3C	Yes	\$3.93	0.56	0.18	Yes	70 μA	1 ms	0°C, +70°C
3.2	Linear Tech	LT1110-12	5V, 10%	12V, 5%	120	76	7; D, L, T, 2R, 2C	Yes	\$4.58	0.45	0.20	Yes	16 μA	1 ms	0°C, +70°C
3.3	Linear Tech	LT1109-12	5V, 10%	12V, 5%	60	84	4; D, L, 2C	Yes	\$3.61	0.38	0.18	Yes	375 μA	1 ms	0°C, +70°C
3.4	Motorola	MC34063A	5V, 10%	12V, 5%	120	75	11; D, L, T, 3C, 5R	Yes	\$2.25	0.49	0.18	Yes	25 μA	2 ms	0°C, +70°C
4.1	Linear Tech	LT1110-12	2V–3.1V	12V, 5%	30	70	7; D, L, T, 2R, 2C	Yes	\$4.71	0.45	0.18	Yes	16 μA	4 ms	0°C, +70°C
4.2	Maxim	MAX732	1.8V–4V	12V, 4%	30	87	9; D, L, 7C,	Yes	\$4.80	0.7	0.18	Yes	45 μA	25 ms	0°C, +70°C
4.3	Maxim	MAX732	1.8V–4V	12V, 4%	60	85	8; D, L, 6C,	No	\$4.15	1.11	0.49	Yes	45 μA	75 ms	0°C, +70°C
5.1	Maxim	MAX658	2V–3.1V	5V, 5%	250	85	7; D, 2L, T, 3C	No	\$4.47	0.92	0.39	Yes	80 μA	25 ms	0°C, +70°C
5.2	Linear Tech	LT1110-5	2V–3.1V	5V, 5%	150	76	7; D, L, T, 2R, 2C	Yes	\$4.72	0.45	0.20	Yes	16 μA	1 ms	0°C, +70°C
6.1	Maxim	MAX667	12.1V–16V	12V, 5%	250	75	3; 2R, C	Yes	\$2.73	0.25	0.15	Yes	0.2 μA	0.1 ms	0°C, +70°C
6.2	Linear Tech	LT1111-12	16V–30V	12V, 5%	120	80	6; 2D, L, 2C, R	Yes	\$3.95	0.78	0.2	No	N/A	N/A	0°C, +70°C
6.3	National	LM294OCT-12	13V–26V	12V, 3%	1A	12/V _{IN}	2; 2C	No	\$1.30	0.5	0.18	No	N/A	N/A	0°C, +70°C
A.1	International Power	NMF0512S	5V, 10%	12V, 5%	80	62	0	No	\$7.90	0.3	0.40	Yes	20 mA	10 μs	-40°C, +70°C
A.2	Shindengen	HDF1212D	8V–16.5V	12V, 5%	120	77	0	No	\$10.00	0.76	0.80	No	N/A	N/A	-10°C, +70°C
A.3	Xentek	NPSC-0512S	5V, 10%	12V, 5%	80	60	2; 2C	No	\$5.50	0.34	0.79	No	N/A	N/A	-10°C, +70°C

NOTES:

1. # External components. D: Diode, L: Inductor, C: Capacitor, R: Resistor, T: Transistor.
2. Cost. Cost estimates assume 10K quantities, based on published pricing at the time this application note was written.
3. PC Area. PC Aarea is conservatively estimated as 2.0x (area of all components). Where actual layouts are presented, the lower value is given. Note that this estimate is for a single sided board, and area can be reduced considerably if both sides of the board are utilized.
4. I Shdn. Current consumed by supply at shutdown. Output settles to V_{CC} at shutdown, so some additional flash V_{PP} leakage/standby will exist.
5. R Time. Rise time from shutdown state. Erase/Writes should not be attempted till V_{PP} level has risen to valid level after shutdown is disabled.

APPENDIX C SOURCES/CONTACTS FOR RECOMMENDED DC-DC CONVERTERS

Linear Technology Corporation

Recommended Products:

- LT1110-12 (DC-DC Converter IC)
- LT1110-5 (DC-DC Converter IC)
- LT1109-12 (DC-DC Converter IC)
- LT1111-12 (DC-DC Converter IC)

In U.S.A.:

1630 McCarthy Blvd.
Milpitas, CA 95035-7487
Tel: (408) 432-1900
Fax: (408) 432-0507

In Europe (U.K.):

111 Windmill Road
Sunbury
Middlesex TW16 7EF
U.K.
Tel (44)(932) 765688
Fax (44)(932) 781936

In Asia (Japan):

4F Ichihashi Bldg
1-8-4 Kudankita Chiyoda-ku
Tokyo 102 Japan
Tel (81) (03) 3237-7891
Fax (81) (03) 3237-8010

Maxim Integrated Products

Recommended Products:

- MAX732 (DC-DC Converter IC)
- MAX658 (DC-DC Converter IC)
- MAX667 (DC-DC Converter IC)

In U.S.A.:

120 San Gabriel Drive
Sunnyvale, CA 94086
Tel (408) 737-7600
Fax (408) 737-7194

In Europe (U.K.):

Maxim Integrated Products (UK), Ltd.
Tel: (44) (734) 845255

In Asia (Japan):

Maxim Japan Co., Ltd.
Tel: 81 (03) 3232-6141

Motorola Semiconductor Inc.

Recommended Product:

- MC34063AD (DC-DC Converter IC)

In U.S.A.:

616 West 24th Street
Tempe, AZ 85282
Tel: (800) 521-6274

In Europe (U.K.):

Tel: (44) (296) 395-252

In Asia (Japan):

Tel: (81) (3) 440-3311

National Semiconductor

Recommended Product:

- LM2940CT-12 (Voltage Regulator IC)

In the U.S.:

2900 Semiconductor Drive
P.O. Box 58090
Santa Clara, CA 95052
Tel: (408) 721-5000

In Europe:

National Semiconductor (UK) Ltd.
The Maple, Kembrey Park
Swindon, Wiltshire SN26UT
U.K.
Tel: (07-93) 614141
Fax: (07-93) 697522

In Asia:

National Semiconductor Japan Ltd.
Sanseido Bldg. 5F
4-15 Nishi Shinjuku
Shinjuku-ku
Tokyo 160 Japan
Tel: (81) (3) 299-7001
Fax: (81) (3) 299-7000

**Newport Components/
International Power****Recommended Product:**

- NMF0512S (5V-12V Converter Module)

In U.S.A.:

International Power Sources
200 Butterfield Drive
Ashland, MA 01721
Tel: (508) 881-7434
Fax: (508) 879-8669

In Europe:

Newport Components
4 Tanners Drive
Blakelands North
Milton Keynes MK14 5NA
Tel: (0908) 615232
Fax: (0908) 617545

Shindengen Electric Co. Ltd.**Recommended Product:**

- HDF0512D (12V unreg. to 12V reg. converter module)

In the U.S.:

2649 Townsgate Road #200
Westlake Village, CA 91361
Tel: (800) 634-3654
Fax: (805) 373-3710

In Europe:

Shindengen Magnaquest U.K. Ltd.
Unit 13, River Road,
Barking Business Park,
33 River Road, Barking,
Essex 1G11 ODA
Tel: (44) (81) 591-8703
Fax: (44) (81) 591-8792

In Asia:

2-1,2-Chome Otemachi
Chiyoda-ku
Tokyo 100
Japan
Tel: (81) (3) 279-4431
Fax: (81) (3) 279-6478

Xentek Inc.**Recommended Product:**

- NPSC0512S (5V-12V Converter Module)

In U.S.A.:

760 Shadowridge Drive
Vista, CA 92083
Tel: (619) 727-0940
Fax: (619) 727-8926

In Europe (Germany):

Xentek, Inc.
c/o Taiyo Yuden GMBH.
Obermaierstrasse 10,
D-8500 Nurnberg 10
Federal Republic of Germany
Tel: (49) (911) 350-8400
Fax: (49) (911) 350-8460

In Asia (Japan):

Xentek, Inc.,
c/o Taiyo Yuden., Ltd.
6-16-20, Ueno, Taito-ku
Tokyo 110
Japan
Tel: (81) (3) 3837-6547
Fax: (81) (3) 3835-4752

APPENDIX D CONTACTS FOR DISCRETE COMPONENTS

Matsuo Electric Co., Ltd.

Matsuo's 267 series surface mount tantalum chip capacitors are recommended by Maxim and Linear Technology for input and output filter capacitors on their DC-DC converters. Part #'s are included on the parts list that accompanies most solutions. If alternate "equivalents" are required, choose high reliability, low ESR (Equivalent Series Resistance) and low ESL (Equivalent Series Inductance) type tantalums, which help in keeping output ripple and switching noise to a minimum.

In U.S.A.:

2134 Main St., Ste. 200
Huntington Beach, CA 92648
Tel: (714) 969-2491
Fax: (714) 960-6492

In Europe:

Steucon - Center II Mergenthaleralle 77
D-6236 Eschben/Ts.
Federal Republic of Germany
Tel: 6196-470-361
Fax: 6196-470-360

In Asia:

Oak Esaka Bldg.
10-28 Hiroshima-Cho
Saita-shi
Osaka 564
Tel: (06) 337-6450
Fax: (06) 337-6456

Sumida Electric Co. Ltd.

Sumida CD series surface mount inductors are recommended by Maxim, Linear Technology for their miniature size and relatively low cost. These are well suited to low power DC-DC converter applications. Contact Sumida Electric directly for procuring these. The part #'s are included in the parts list that accompanies most solutions. In applications where noise (EMI) is a concern, shielded varieties are also offered by Sumida.

In U.S.A.:

637 East Golf Road
Suite 209
Arlington Heights, IL 60005
Tel: (708) 956-0666
Fax: (708) 956-0702

In Asia:

4-8 Kanamachi 2-chome,
Katsushika-ku,
Tokyo 125
Japan
Tel: (81) (03) 3607-5111
Fax: (81) (03) 3607-5428

Coiltronix Inc.

Coiltronix is recommended as a good alternate source for surface mount inductors. The CTX series offered by Coiltronix is well suited to DC-DC converter applications. These are shielded, and have a toroidal core. However, they are bigger in size and currently much more expensive (7X to 8X) than the Sumida varieties recommended in the solutions herein. The equivalent part numbers are:

Sumida CD54-470 → Coiltronix CTX50-1
Sumida CD54-180 → Coiltronix CTX20-1
Sumida CD54-220 → Coiltronix CTX20-1
Sumida CD75-470 → Coiltronix CTX50-2
Sumida CDR105-470 → Coiltronix CTX50-2

In U.S.A.:

Coiltronix Inc.
984 S.W. 13th Court
Pompano Beach, FL 33069
Tel: (305) 781-8900
Fax: (305) 782-4163

In U.K.:

Microelectronics Technology Ltd.
Great Haseley Trading Estate
Great Haseley
Oxfordshire OX9 7PF
U.K.
Tel: (08) 44 278781
Fax: (08) 44 278746

In Asia:

Serial System Mktg.
Poh Leng Bldg., #02-01
21 Moonstone Lane
Singapore 1232
Tel: 2938830
Fax: 2912673

Coilcraft

Coilcraft is also recommended as a good alternate source for surface mount inductors. The N2724-A shielded series is well suited to DC-DC converter applications. These are bigger and currently more expensive (2x to 3x) than the Sumida inductors recommended in the solutions. Contact Coilcraft directly for any applications assistance or for procurement of these parts. The equivalent part numbers are:

Sumida CD54-470 → Coilcraft N2724-A 47 μ H
Sumida CD54-180 → Coilcraft N2724-A 18 μ H
Sumida CDR105-470 → Coilcraft N2724-A 47 μ H

In the US:

1102 Silver Lake Road
Cary, IL 60013
Tel: (708) 639-6400
Fax: (708) 639-1469

In Europe:

21 Napier Place
Wardpark North
Cumbernauld
Scotland G68 0LL
Tel: 0236 730595
Fax: 0236 730627

In Asia:

Block 101, Boon Keng Road
#06-13/20
Kallang Basin Industrial Estate
Singapore 1233
Tel: 2966933
Fax: 2964463

Philips Components

Philips Components is recommended as a good source for surface mount (SMD) resistors (standard 9C series, and 9B (MELF) series). Part #'s are included in the parts list that accompanies most of the solutions in the application note. Many alternate sources exist.

In the US:

2001 W. Blue Heron Blvd.
P.O. Box 10330
Riviera Beach, FL 33404
Tel: (407) 881-3200
Fax: (407) 881-3304

In Europe:

Philips Components Ltd.
Mullard House
Torrington Place
London WC1E 7HD
Tel: (44) 71 580 6633
Fax: (44) 71 636 0394

In Asia:

Philips K.K.
Philips Bldg. 13-37
Kohman 2-chome
Minato-Ku Tokyo 108
Tel: (81) 3 740-5028
Fax: (81) 3 740-5035

Siliconix-Logic Level PFETs

Siliconix offers low-“on” resistance logic level PFETs (Si9400, and Si9405) that can be used for switching a DC-DC converter into a shutdown state by using these switches on the high side of the input to the converter (see Appendix E).

In the US:

2201 Laurelwood Road
P.O. Box 54951
Santa Clara, CA 95056-9951
Tel: (408) 988-8000
Fax: (408) 727-5414

In Europe:

Weir House
Overbridge Square, Hambridge Lane
Newbury, Berks RG14 5UX
Tel: (0635) 30905
Fax: (0635) 34805

In Asia:

Room 709, Chinachem Golden Plaza
77 Mody Road
TST East Kowloon
Tel: (852) 724-3377
Fax: (852) 311-7909

APPENDIX E

OTHER DESIGN CONSIDERATIONS

E.1 VPP Valid Handshake Logic

It is often desirable to have, along with the V_{PP} solution, a handshake signal (using extra hardware) that is asserted as long as the voltage level on V_{PP} is valid. The following schematic illustrates a good way of achieving this. This handshake signal could be used to determine when it is suitable to perform writes/erases on the flash device. The circuit shown uses a precision zener voltage reference and a comparator, along with bias resistors, to monitor the voltage level on V_{PP}. The point at which the comparator trips must be set after careful consideration of the variation in the reference voltage and the tolerances on the bias resistors. The worst case conditions on these variations must guarantee that the handshake signal is asserted when V_{PP} is at its worst case lower-end level (11.4V). Care must be taken to use the exact same components as specified in order to maintain the tight tolerance on the trip level of the output signal.

E.2 Obtaining Shutdown Using Logic Level PFETs

Low "on" resistance logic level PFETs can be used on the high side of the input to the DC-DC converters to obtain shutdown. One such part is the Si9405 from Siliconix Inc. The device is part of the "little foot" series, and is available in an SO8 (8-pin surface mount) package. The Si9405 is a logic level PFET with an "on re-

sistance" of 0.2Ω (at a gate drive of 4.5V). It is important to have as low an "on" resistance as possible, since the peak currents and start-up currents into the supply are high. Care must be taken to ensure that the DC-DC conversion process is not affected after accounting for the drop in input voltage across the PFET.

E.3 Working of the Discrete Step Up Switching Regulator

This section presents a brief overview of the operation of discrete step up switching regulators, and presents issues that the user needs to be concerned with while designing these solutions into the system.

The four most basic elements of a discrete switching regulator power supply are:

1. The SMPS IC (which includes the switch control element and logic, along with the power switch itself),
 2. An inductor for storage and transfer of energy between the input and output,
 3. A switching diode to direct the inductor energy to "catch", or channel, the inductor energy to the output, and
 4. An output filter capacitor.

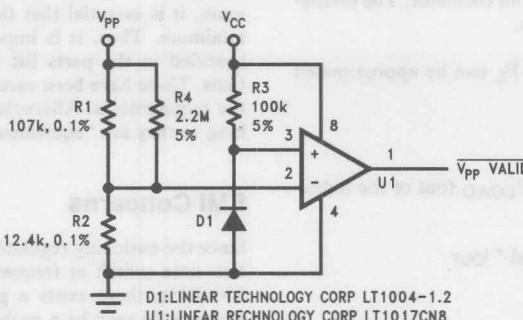


Figure E-1 Vpp Valid Handshake Circuit

In the boost configuration where the output voltage is greater than the input voltage, the basic switching power supply configuration is as shown in Figure E.2:

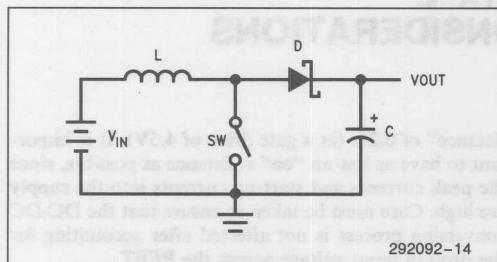


Figure E-2. Working of the Step-Up Switching Regulator

The power switch SW can be turned on and off; the control for it is derived from a feedback mechanism that senses the output voltage. While the switch is turned on, the inductor stores energy as the current flows through it from the input supply. The peak current through the inductor I_L can be approximated as $(V_{IN}/L * t_{ON})$; where t_{ON} is the on time of the switch. During this time, the energy is supplied by the input voltage, $V_L = V_{IN}$. The output is isolated from the inductor via the reverse-biased diode, and the load current is supplied by the output filter capacitor. When the switch turns off, the energy stored in the inductor appears as a rapidly increasing voltage across the inductor. As soon as this voltage reaches a value equal to the output voltage plus the voltage drop across the diode, the diode switches on and current starts to flow through the diode. This diode current supplies the load current while also at the same time charging up the output filter capacitor to the output voltage.

The switch is controlled by sensing the output voltage via a feedback mechanism—usually a pair of resistors. This sense voltage is gated via a comparator whose output acts as a control signal to an oscillator. The oscillator output controls the switch.

The power into the inductor P_L can be approximated as:

$$P_L = 0.5 * L * I_{PK}^2 * f_{OSC}$$

and the power into the load P_{LOAD} (out of the inductor) can be approximated as

$$P_{LOAD} = (V_{OUT} + V_D - V_{IN}) * I_{OUT}$$

The peak currents through the inductor is usually several times higher than the load current, is mostly of the value of the load current and builds up during time t_{ON} . On most of the solutions presented here, peak operating currents lie in the range of 500 mA to 1.2A. Though this may seem high, most of this in-rush of energy is transferred to the output, and little is lost to heat due to the efficient energy storage characteristic of inductors. Note that since the peak currents are high, the input voltage source must be capable of providing this current, and the current capability of the input source must not be calculated simply as $(V_{OUT} * I_{OUT})/(V_{IN} * \text{Eff})$. A large bypass capacitor at the input pin of the converter is hence also necessary on all designs.

Some of the solutions presented in this application note are of the fixed duty cycle or fixed on time type (e.g. LT110-12, LT1109-12, MC34063A), whereas some of them vary the duty cycle depending on the load current (e.g. MAX732, MAX658). These latter ones provide higher efficiencies.

Inductor Selection

The choice of an inductor is crucial to the design of the power supply system. To begin with, the inductor value must be low enough to supply the peak currents needed when the input voltage V_{IN} , as well as the on time t_{on} , are at their worst case low value. On the other hand, the inductor value must be high enough so that the peak currents at the worst case high values do not exceed the maximum peak currents that can be handled by the switch. Furthermore, once the value has been picked, the physical inductor that is chosen for the job must be able to handle these peak currents, and must not saturate. This is done by picking an inductor whose DC current rating is more than the worst case peak current that will be required by the operation of the device. The other characteristic to consider is the resistance of the inductor. In order to keep losses to a minimum, it is essential that the resistance of the coil is a minimum. Thus, it is important to use the inductors specified in the parts list that accompanies the solutions. These have been carefully chosen after reviewing the requirements. Alternate inductors may be used, as long as they are “equivalent”.

EMI Concerns

Since the switching regulators presented in this application note switch at frequencies between 60 KHz and 200 KHz, there exists a potential for EMI. In cases where EMI may be a problem, shielded inductors can be used. This will reduce EMI significantly. Shielded versions of the inductors specified are readily available. Contact the vendor directly for these.

Output Switching Noise

Output switching noise has several sources. The most significant one is the IR drop through the ESR (Equivalent Series Resistance) of the output filter capacitor. This is caused by switching current pulses from the inductor. There is also noise in the form of switching spikes riding on the DC output. This is due to the output filter capacitor's ESL (Equivalent Series Inductance), current spikes in the ground trace and rectifier turn-on transients.

It is important to use low ESR and low ESL output and input filter capacitors. Proper layout is also essential in

order to avoid spikes in the output. The safest solution is to use a filter circuit at the output. LC filters are not recommended, because of the transient nature of the load currents on flash devices. An RC filter is recommended on most solutions as an option. Two 1Ω resistors are used in parallel to avoid causing a significant drop across the resistance. This method is inexpensive and assures that the spikes riding on the output waveform are contained to within the 5% tolerance requirement on V_{pp}.

In addition, care must be taken to keep the leads from the output of the solution to all flash devices as short as possible. Use of a $0.1 \mu F$ capacitor at the V_{pp} pin of each flash device is highly recommended.

APPENDIX F PC LAYOUTS FOR SOME RECOMMENDED SOLUTIONS

F.1 Maxim Integrated Products MAX732

The double-sided layout presented below (Figure F-1) has been designed for the MAX732 5V–12V converter solution (Section 3.1). It is a double sided layout and has been designed for the parts specified in the parts list that accompanies the solution. Contact Maxim for any additional layout assistance.

F.2 Linear Technology Corporation LT1110-12

The single-sided layout presented below (Figure F-2) can be used to implement the LT1110-12 5V to 12V

converter (Section 3.2), the LT1110-12 3V–12V converter (Section 4.1), or the LT1110-5 3V to 5V converter (Section 5.2). The layout has been designed for the parts that are specified in the parts list that accompanies these solutions. Contact Linear Technology for any additional layout assistance.

F.3 Linear Technology Corporation LT1109-12

The single-sided layout presented below (Figure F-3) can be used to implement the LT1109-12 5V–12V converter solution (Section 3.3). The layout has been designed for the parts that are specified in the parts list that accompanies the solution. Contact Linear Technology for any additional layout assistance.

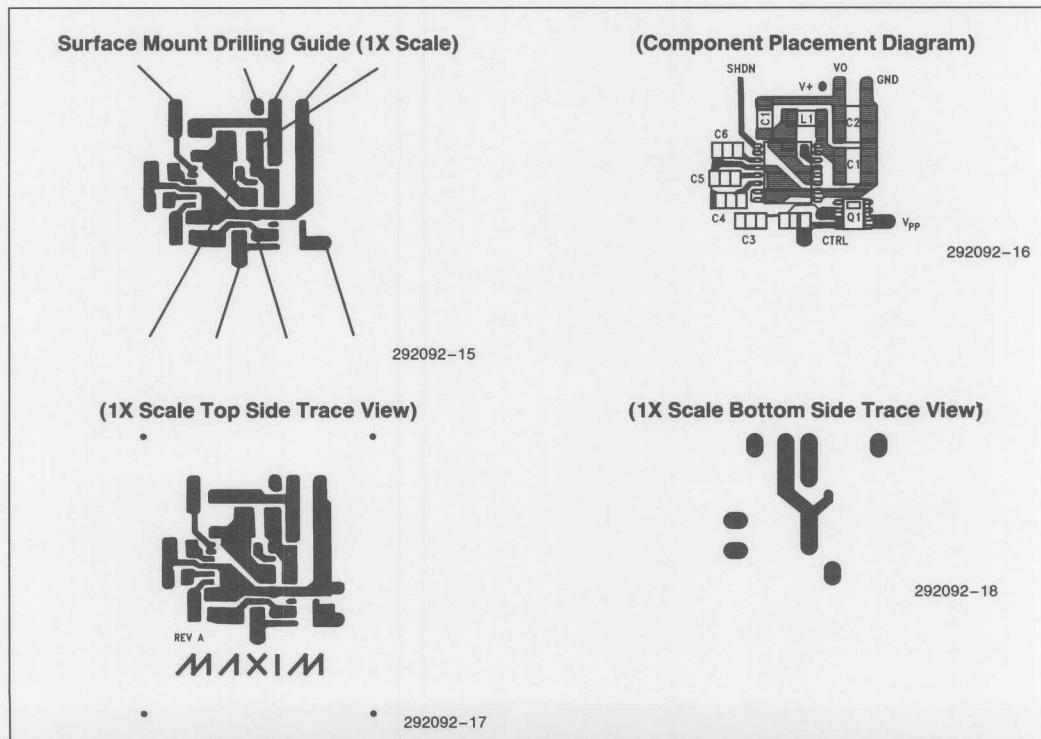


Figure F-1

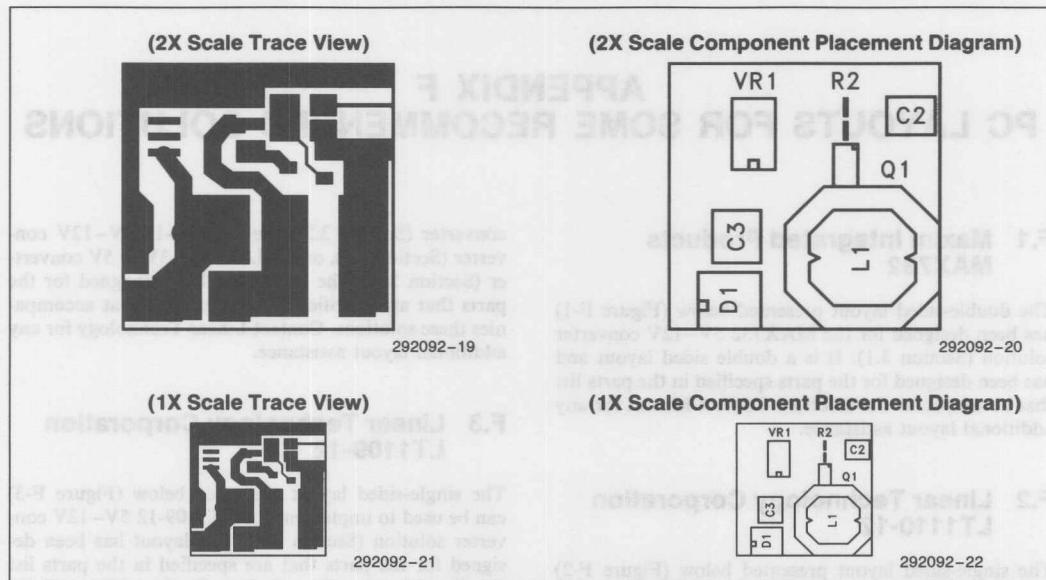
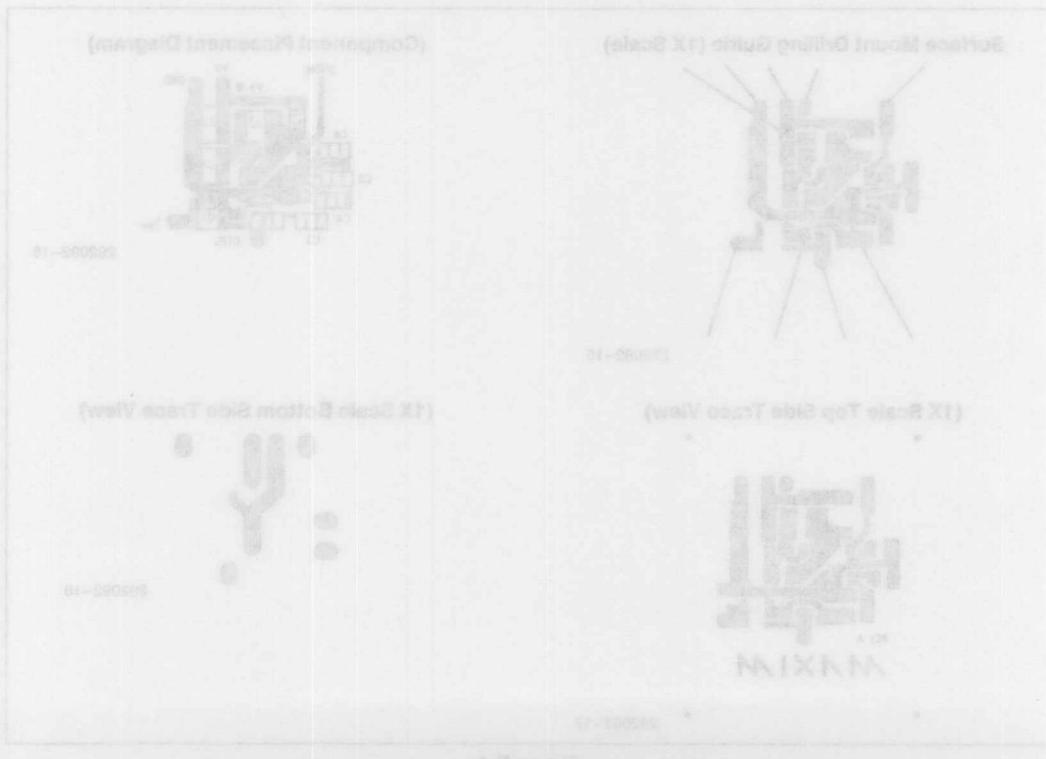
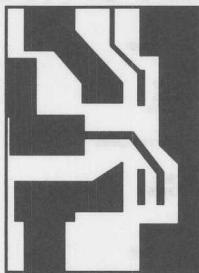


Figure F-2



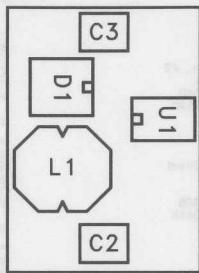


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(1X Scale Trace View)

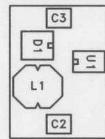


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292092-26

(1X Scale Component Placement Diagram)



292092-28

Figure F-3



NORTH AMERICAN SALES OFFICES

ALABAMA

Intel Corp.
5015 Bradford Dr., #2
Huntsville 35805
Tel: (205) 830-4010
FAX: (205) 837-2640

ARIZONA

Intel Corp.
410 North 44th Street
Suite 500
Phoenix 85008
Tel: (602) 231-0386
FAX: (602) 244-0446

CALIFORNIA

Intel Corp.
21515 Vanowen Street
Suite 116
Canoga Park 91303
Tel: (818) 704-8500
FAX: (818) 340-1144

Intel Corp.
1 Sierra Gate Plaza
Suite 280C
Roseville 95678
Tel: (916) 782-8086
FAX: (916) 782-8153

Intel Corp.
9665 Chesapeake Dr.
Suite 325
San Diego 92123
Tel: (619) 292-8086
FAX: (619) 292-0628

*Intel Corp.
400 N. Tustin Avenue
Suite 450
Santa Ana 92705
Tel: (714) 835-9642
TWX: 910-595-1114
FAX: (714) 541-9157

*Intel Corp.
San Tomas 4
2700 San Tomas Expressway
2nd Floor
Santa Clara 95051
Tel: (408) 986-8086
TWX: 910-338-0255
FAX: (408) 727-2620

COLORADO

Intel Corp.
4445 Northpark Drive
Suite 100
Colorado Springs 80907
Tel: (719) 594-6622
FAX: (303) 594-0720

*Intel Corp.
600 S. Cherry St.
Suite 700
Denver 80222
Tel: (303) 321-8086
TWX: 910-931-2289
FAX: (303) 322-8670

CONNECTICUT

Intel Corp.
301 Lee Farm Corporate Park
83 Wooster Heights Rd.
Danbury 06810
Tel: (203) 748-3130
FAX: (203) 794-0339

FLORIDA

Intel Corp.
800 Fairway Drive
Suite 160
Deerfield Beach 33441
Tel: (305) 421-0506
FAX: (305) 421-2444

*Intel Corp.
5850 T.G. Lee Blvd.
Suite 340
Orlando 32822
Tel: (407) 240-8000
FAX: (407) 240-8097

ILLINOIS

*Intel Corp.
Woodfield Corp. Center III
300 N. Martingale Road
Suite 400
Schaumburg 60173
Tel: (708) 605-8031
FAX: (708) 706-9762

INDIANA

Intel Corp.
8910 Purdue Road
Suite 350
Indianapolis 46268
Tel: (317) 875-0623
FAX: (317) 875-8938

MARYLAND

*Intel Corp.
10010 Junction Dr.
Suite 200
Annapolis Junction 20701
Tel: (301) 206-2860
FAX: (301) 206-3677
(301) 206-3678

MASSACHUSETTS

*Intel Corp.
Westford Corp. Center
3 Carlisle Road
2nd Floor
Westford 01886
Tel: (508) 692-0960
TWX: 710-343-6333
FAX: (508) 692-7867

MICHIGAN

Intel Corp.
7071 Orchard Lake Road
Suite 100
West Bloomfield 48322
Tel: (313) 851-8096
FAX: (313) 851-8770

MINNESOTA

Intel Corp.
3500 W. 80th St.
Suite 360
Bloomington 55431
Tel: (612) 835-6722
TWX: 910-576-2867
FAX: (612) 831-6497

NEW JERSEY

*Intel Corp.
Lincroft Office Center
125 Half Mile Road
Red Bank 07701
Tel: (908) 747-2233
FAX: (908) 747-0983

NEW YORK

*Intel Corp.
850 Crosskeys Office Park
Fairport 14450
Tel: (716) 425-2750
TWX: 510-253-7391
FAX: (716) 223-2561

*Intel Corp.
2950 Express Dr., South
Suite 130
Islandia 11722
Tel: (516) 231-3300
TWX: 510-227-6236
FAX: (516) 348-7939

*Intel Corp.
300 Westgate Business Center
Suite 230
Fishkill 12524
Tel: (914) 897-3860
FAX: (914) 897-3125

OHIO

*Intel Corp.
3401 Park Center Drive
Suite 220
Dayton 45414
Tel: (513) 890-5350
TWX: 810-450-2528
FAX: (513) 890-8658

*Intel Corp.
25700 Science Park Dr.
Suite 100
Beachwood 44122
Tel: (216) 464-2736
TWX: 810-427-9298
FAX: (804) 282-0673

OKLAHOMA

Intel Corp.
6801 N. Broadway
Suite 115
Oklahoma City 73162
Tel: (405) 848-8086
FAX: (405) 840-9819

OREGON

*Intel Corp.
15254 N.W. Greenbrier Pkwy.
Building B
Beaverton 97006
Tel: (503) 645-8051
TWX: 910-467-8741
FAX: (503) 645-8181

PENNSYLVANIA

*Intel Corp.
925 Harvest Drive
Suite 200
Blue Bell 19422
Tel: (215) 641-1000
FAX: (215) 641-0785

*Intel Corp.
400 Penn Center Blvd.
Suite 610
Pittsburgh 15235
Tel: (412) 823-4970
FAX: (412) 829-7578

PUERTO RICO

Intel Corp.
South Industrial Park
P.O. Box 910
Las Piedras 00671
Tel: (809) 733-8616

TEXAS

Intel Corp.
8911 N. Capital of Texas Hwy.
Suite 4230
Austin 78759
Tel: (512) 794-8086
FAX: (512) 338-9335

*Intel Corp.
12000 Ford Road
Suite 400
Dallas 75234
Tel: (214) 241-8087
FAX: (214) 484-1180

*Intel Corp.
7322 S.W. Freeway
Suite 1490
Houston 77074
Tel: (713) 988-8086
TWX: 910-881-2490
FAX: (713) 988-3660

UTAH

Intel Corp.
428 East 6400 South
Suite 104
Murray 84107
Tel: (801) 268-1457

WASHINGTON

Intel Corp.
155 108th Avenue N.E.
Suite 100
Bellevue 98004
Tel: (206) 453-3002
TWX: 910-443-3002
FAX: (206) 451-9556

Intel Corp.
408 N. Mullan Road
Suite 102
Spokane 99206
Tel: (509) 928-8086
FAX: (509) 928-9467

WISCONSIN

Intel Corp.
330 S. Executive Dr.
Suite 102
Brookfield 53005
Tel: (414) 784-2015
FAX: (414) 796-2115

CANADA

BRITISH COLUMBIA
Intel Semiconductor of
Canada, Ltd.
4585 Canada Way
Suite 202
Burnaby V5G 4L6
Tel: (604) 298-0387
FAX: (604) 298-8234

ONTARIO

Intel Semiconductor of
Canada, Ltd.
2650 Queenview Drive
Suite 500
Ottawa K2B 8H6
Tel: (613) 829-9714
FAX: (613) 820-5936

Intel Semiconductor of
Canada, Ltd.
190 Attwell Drive
Suite 500
Richmond M6V 6H8
Tel: (416) 675-2105
FAX: (416) 675-2438

QUEBEC

Intel Semiconductor of
Canada, Ltd.
1 Rue Holiday
Suite 115
Tour East
Pt. Claire H9R 5N3
Tel: (514) 694-9130
FAX: 514-694-0064

[†]Sales and Service Office

^{*}Field Application Location